
Optimal Disturbances in Compressible Boundary Layers – Complete Energy Norm Analysis

Simone Zuccher & Anatoli Tumin

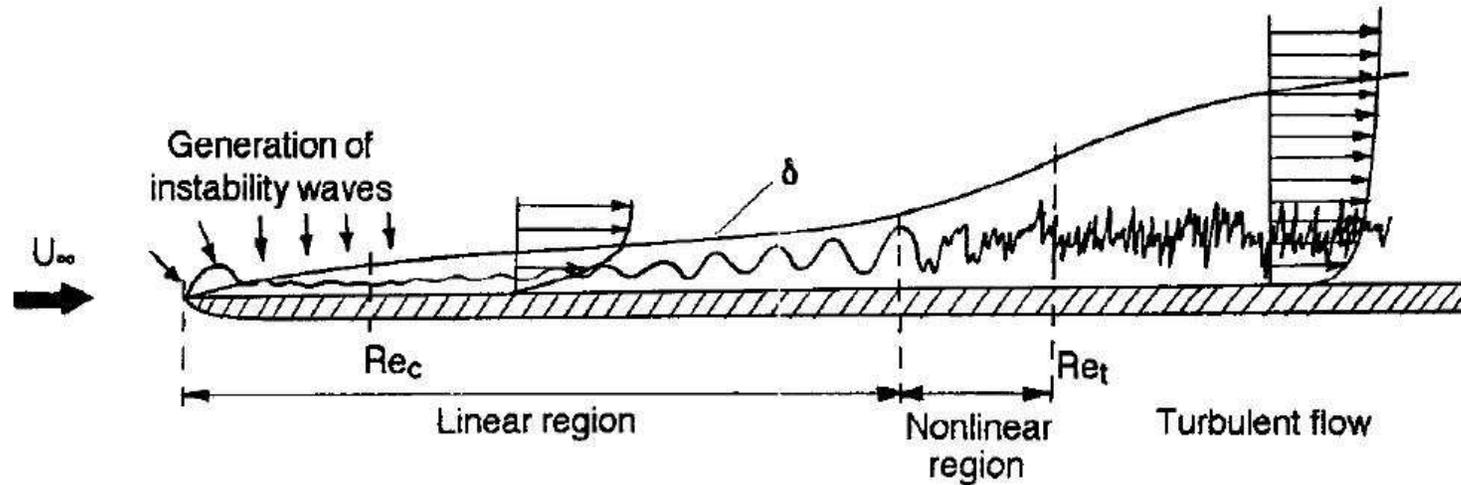
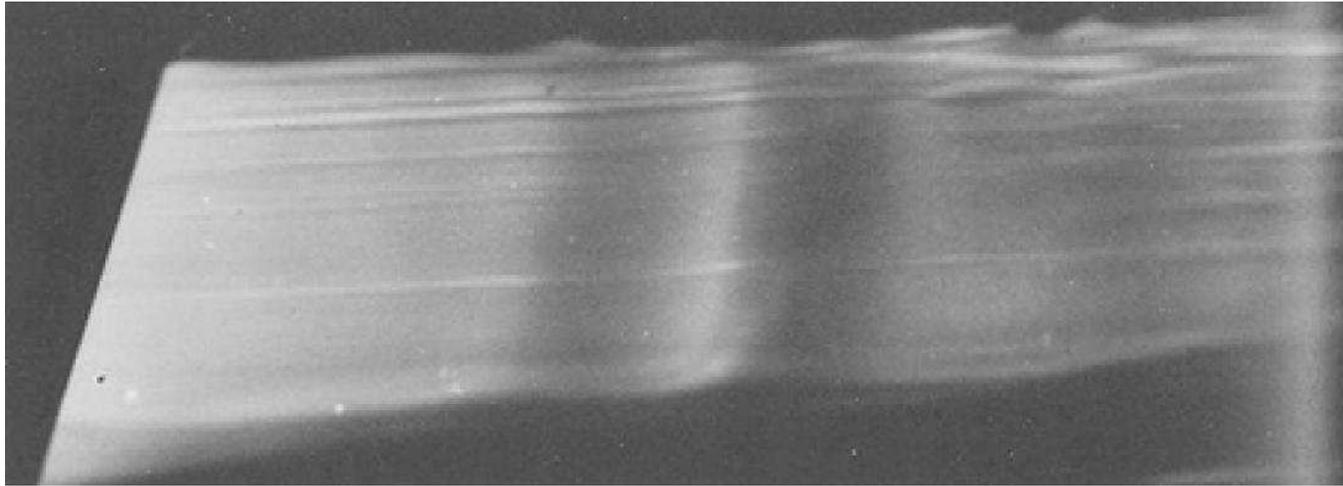
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4th AIAA Theoretical Fluid Mechanics Meeting, 6–9 June, 2005,
Westin Harbour Castle, Toronto, Ontario, Canada.

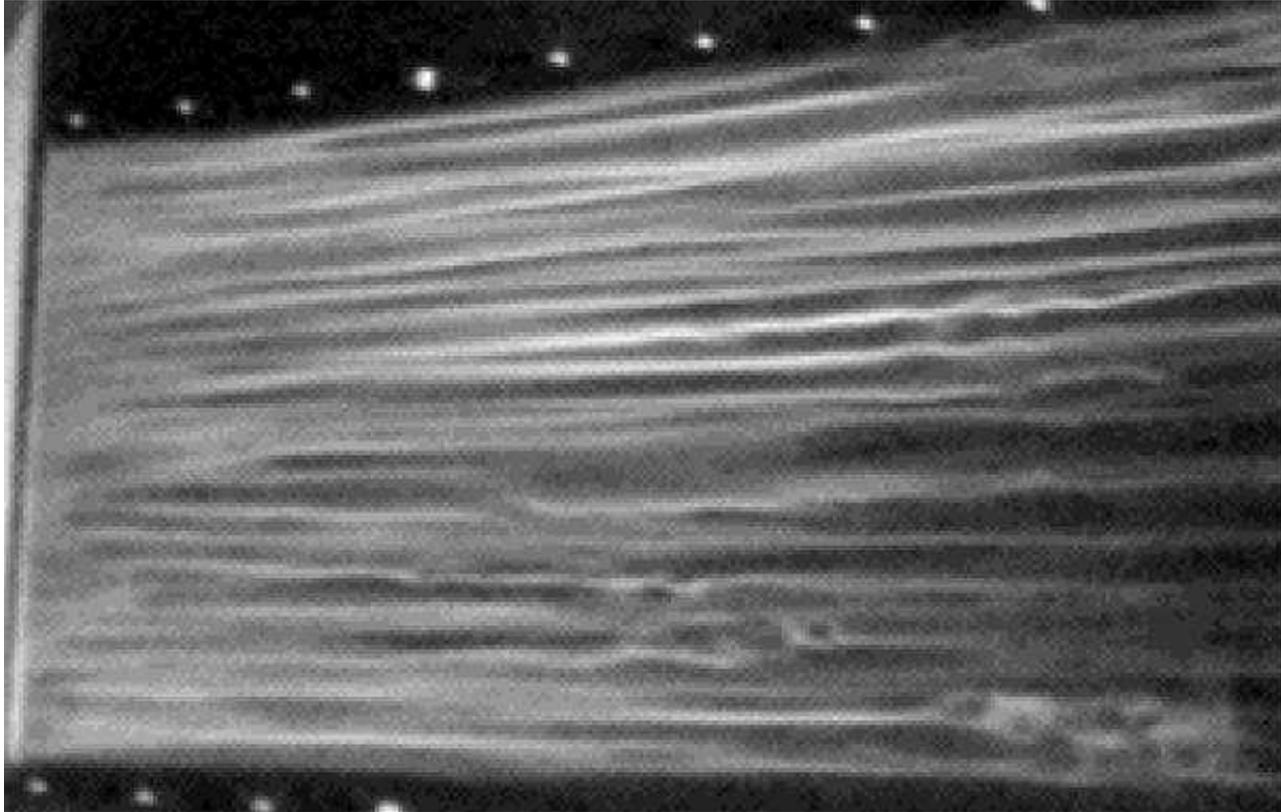
A classical transition mechanism



Tollmien-Schlichting (TS) waves first experimentally detected by Schubauer and Skramstad (1947), “Laminar boundary-layer oscillations and transition on a flat plate”, *J. Res. Nat. Bur. Stand* 38:251–92, originally issued as NACA-ACR, 1943.

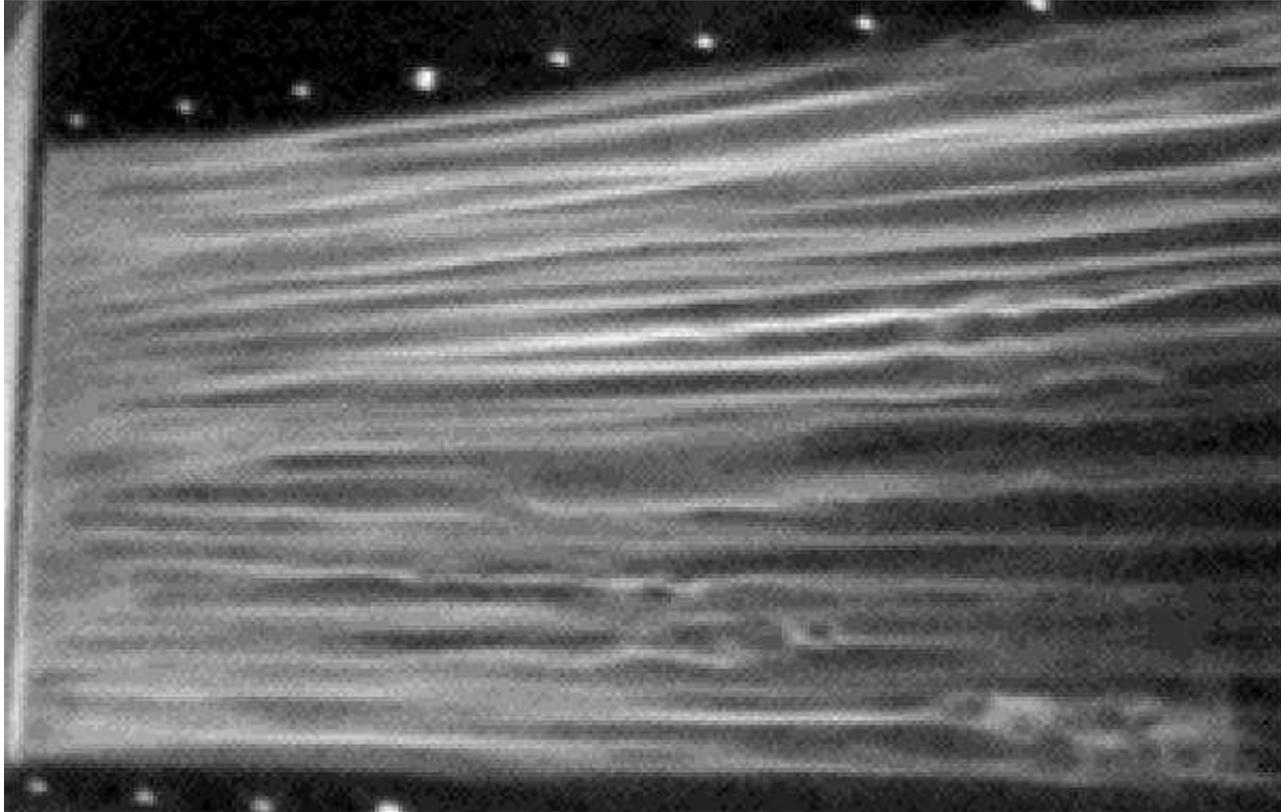
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If the disturbances are not really infinitesimal (real world!)



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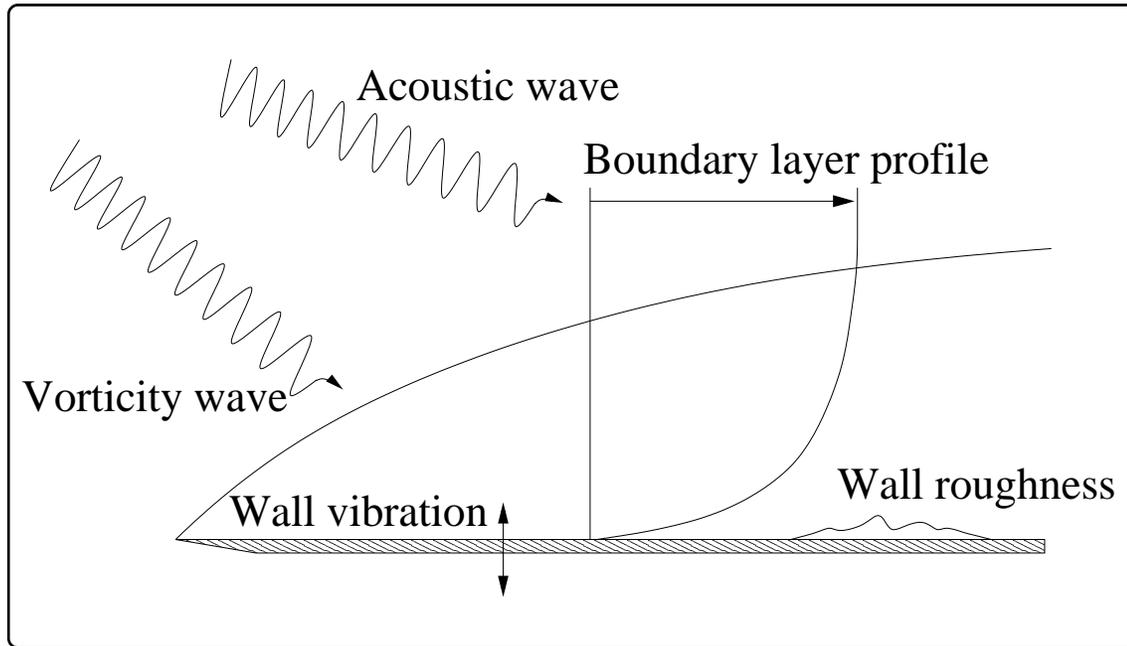
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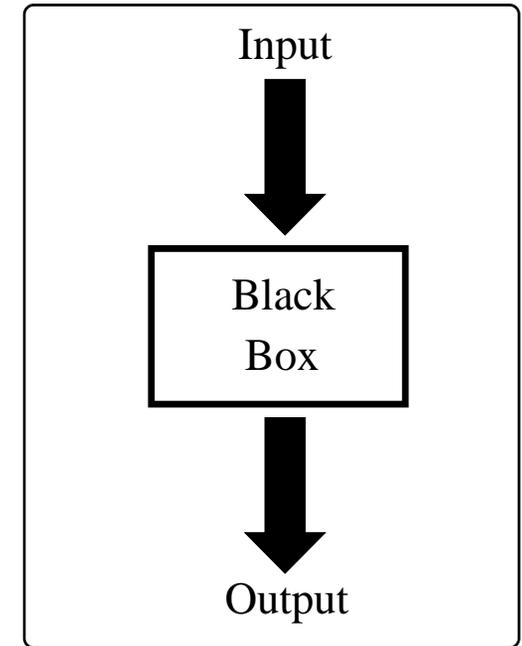
...streaks (instead of waves) can develop where the flow is stable according to the classical neutral stability curve.

Alternative mechanism to TS waves: **Transient growth**.

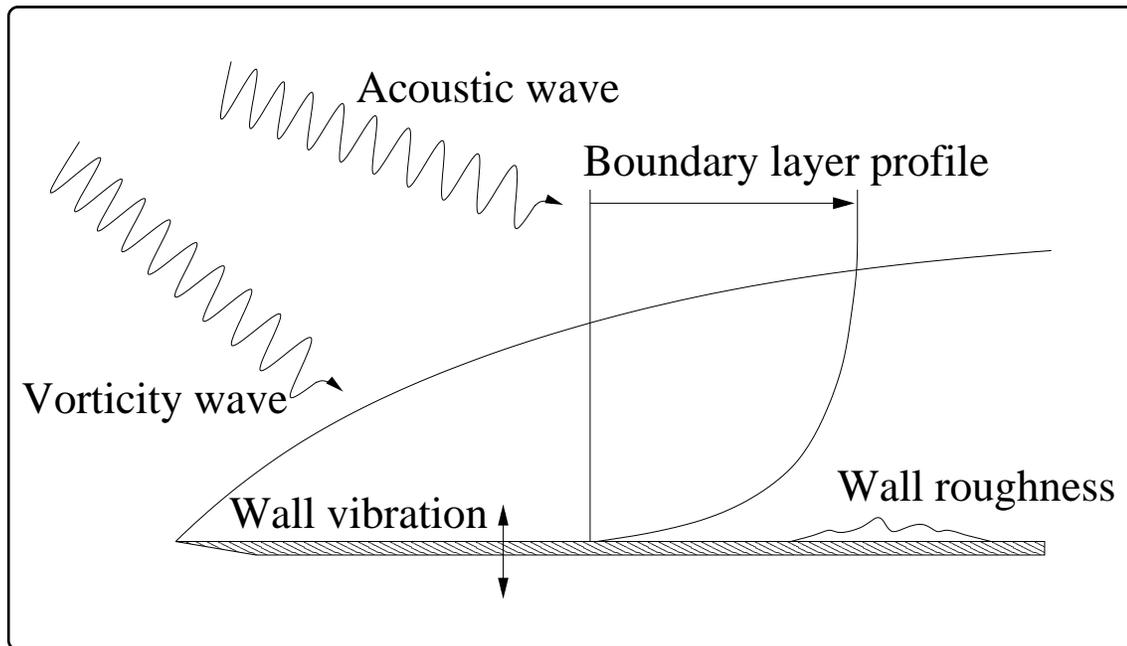
Modelling



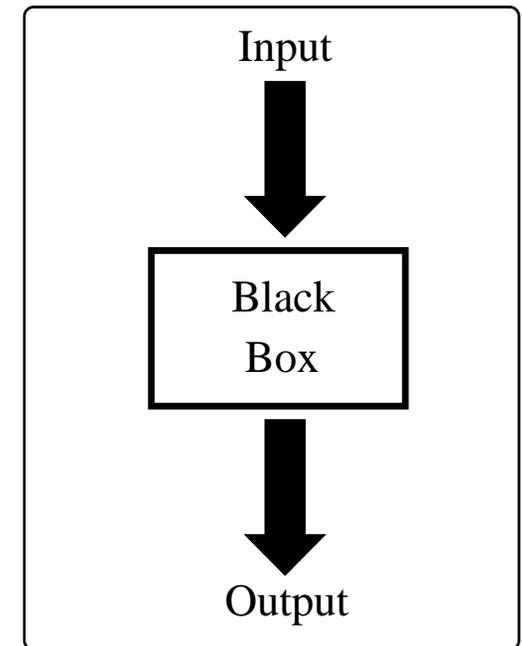
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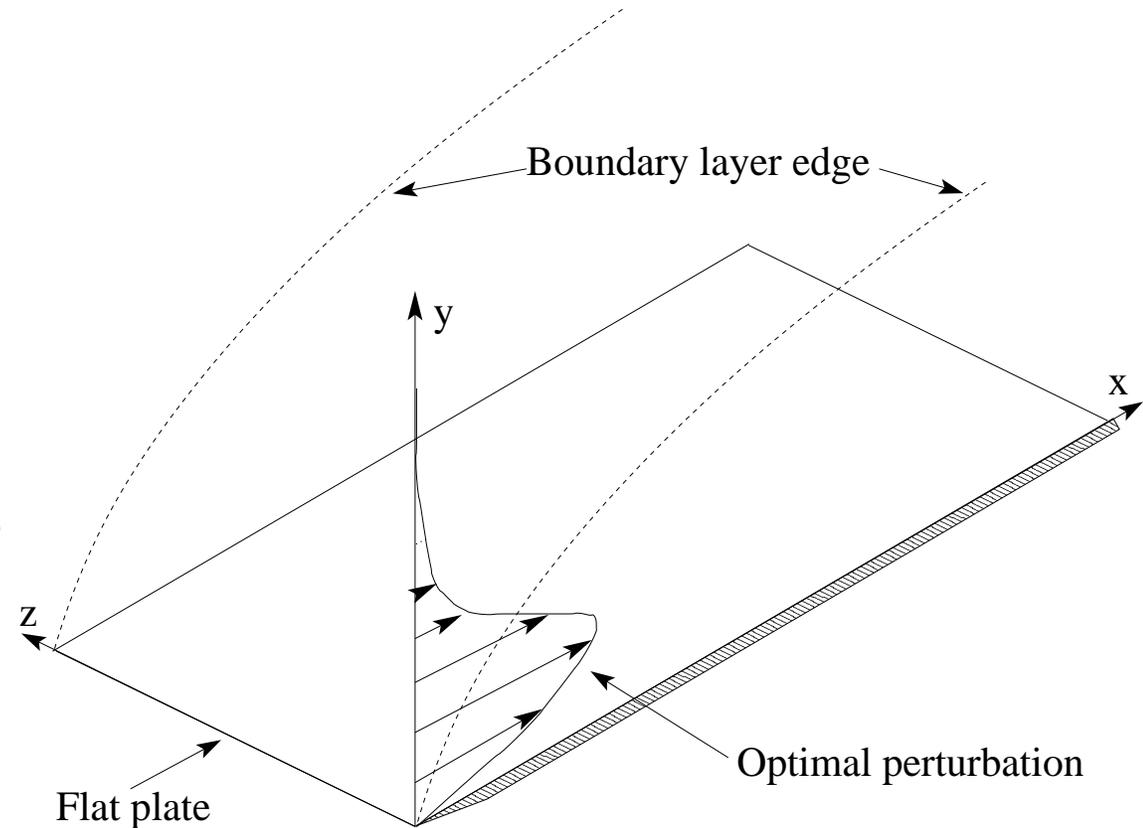
A boundary layer, and its governing equations, can be thought in an **input/output** fashion.

- *Inputs*. Initial conditions and boundary conditions.
- *Outputs*. Flow field, which can be measured by a norm.

Optimal perturbations

Question.

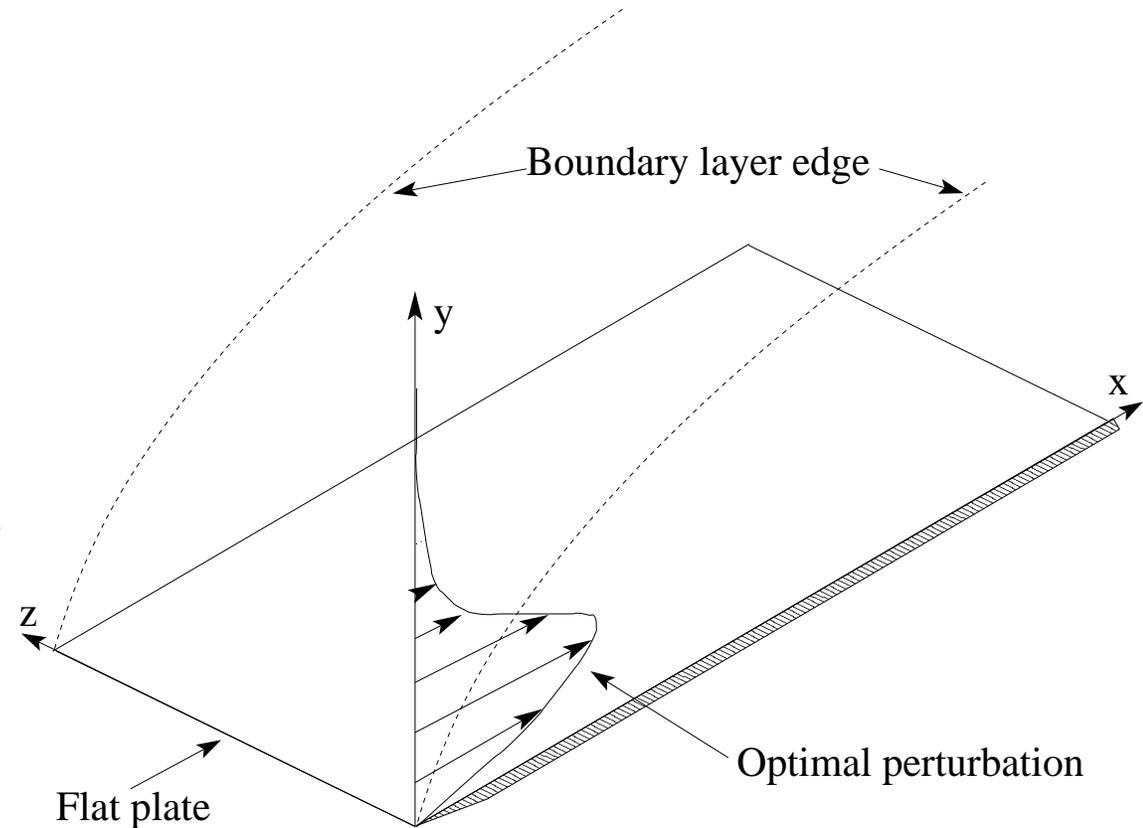
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In this sense the **perturbations** are **optimal**.

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- **Iterative algorithm** for the determination of optimal initial condition.

Problem formulation

- Geometry. Flat plate and sphere.

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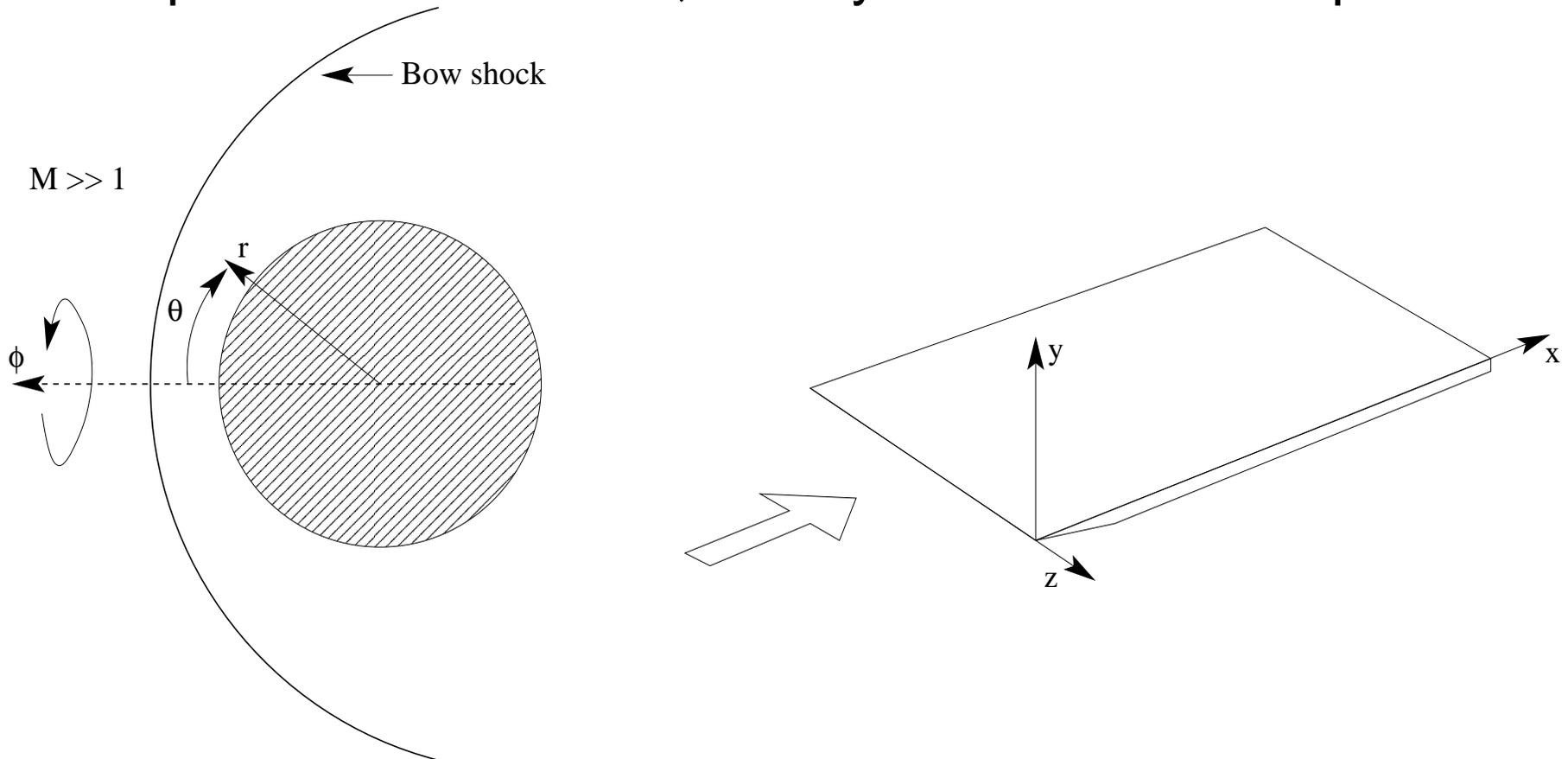
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By assuming perturbations in the form $q(x, y) \exp(i\beta z)$ (flat plate – β spanwise wavenumber) and $q(x, y) \exp(im\phi)$ (sphere – m azimuthal index)...

Governing equations

$$(A\mathbf{f})_x = (D\mathbf{f}_y)_x + B_0\mathbf{f} + B_1\mathbf{f}_y + B_2\mathbf{f}_{yy}$$

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More compactly

$$(\mathbf{H}_1\mathbf{f})_x + \mathbf{H}_2\mathbf{f} = 0$$

with $\mathbf{H}_1 = \mathbf{A} - \mathbf{D}(\cdot)_y$; $\mathbf{H}_2 = -\mathbf{B}_0 - \mathbf{B}_1(\cdot)_y - \mathbf{B}_2(\cdot)_{yy}$

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Mack's energy norm (derived for flat plate and temporal problem), after scaling and using state equation,

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Initial energy of the perturbation

$$E_{\text{in}} = \int_0^{\infty} \left[\rho_{s\text{in}} (v_{\text{in}}^2 + w_{\text{in}}^2) \right] dy \Rightarrow E_{\text{in}} = \int_0^{\infty} \left(\mathbf{f}_{\text{in}}^T \widetilde{\mathbf{M}}_{\text{in}} \mathbf{f}_{\text{in}} \right) dy$$

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- constraint $E_{\text{in}} = E_0 \Rightarrow \mathbf{f}_0^T \mathbf{M}_0 \mathbf{f}_0 = E_0$
- governing equations (BC included) $\mathbf{C}_{n+1} \mathbf{f}_{n+1} = \mathbf{B}_n \mathbf{f}_n$

The augmented functional \mathcal{L} is

$$\mathcal{L}(\mathbf{f}_0, \dots, \mathbf{f}_N) = \mathbf{f}_N^T \mathbf{M}_N \mathbf{f}_N + \lambda_0 [\mathbf{f}_0^T \mathbf{M}_0 \mathbf{f}_0 - E_0] + \sum_{n=0}^{N-1} [\mathbf{p}_n^T (\mathbf{C}_{n+1} \mathbf{f}_{n+1} - \mathbf{B}_n \mathbf{f}_n)]$$

with λ_0 and (vector) \mathbf{p}_n Lagrangian multipliers.

Constrained optimization (2/3)

By adding and subtracting $\mathbf{p}_{n+1}^T \mathbf{B}_{n+1} \mathbf{f}_{n+1}$ in the summation,

$$\begin{aligned} \sum_{n=0}^{N-1} \left[\mathbf{p}_n^T (\mathbf{C}_{n+1} \mathbf{f}_{n+1} - \mathbf{B}_n \mathbf{f}_n) \right] &= \sum_{n=0}^{N-1} \left[\mathbf{p}_n^T \mathbf{C}_{n+1} \mathbf{f}_{n+1} - \mathbf{p}_{n+1}^T \mathbf{B}_{n+1} \mathbf{f}_{n+1} \right] + \\ &\quad \sum_{n=0}^{N-1} \left[\mathbf{p}_{n+1}^T \mathbf{B}_{n+1} \mathbf{f}_{n+1} - \mathbf{p}_n^T \mathbf{B}_n \mathbf{f}_n \right] \\ &= \sum_{n=0}^{N-1} \left[\mathbf{p}_n^T \mathbf{C}_{n+1} \mathbf{f}_{n+1} - \mathbf{p}_{n+1}^T \mathbf{B}_{n+1} \mathbf{f}_{n+1} \right] + \\ &\quad \mathbf{p}_N^T \mathbf{B}_N \mathbf{f}_N - \mathbf{p}_0^T \mathbf{B}_0 \mathbf{f}_0, \end{aligned}$$

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Stationary condition

$$\delta \mathcal{L} = 0 \Rightarrow \frac{\delta \mathcal{L}}{\delta \mathbf{f}_0} \delta \mathbf{f}_0 + \sum_{n=0}^{N-2} \left[\frac{\delta \mathcal{L}}{\delta \mathbf{f}_{n+1}} \delta \mathbf{f}_{n+1} \right] + \frac{\delta \mathcal{L}}{\delta \mathbf{f}_N} \delta \mathbf{f}_N = 0$$

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7. repeat from step 2 on

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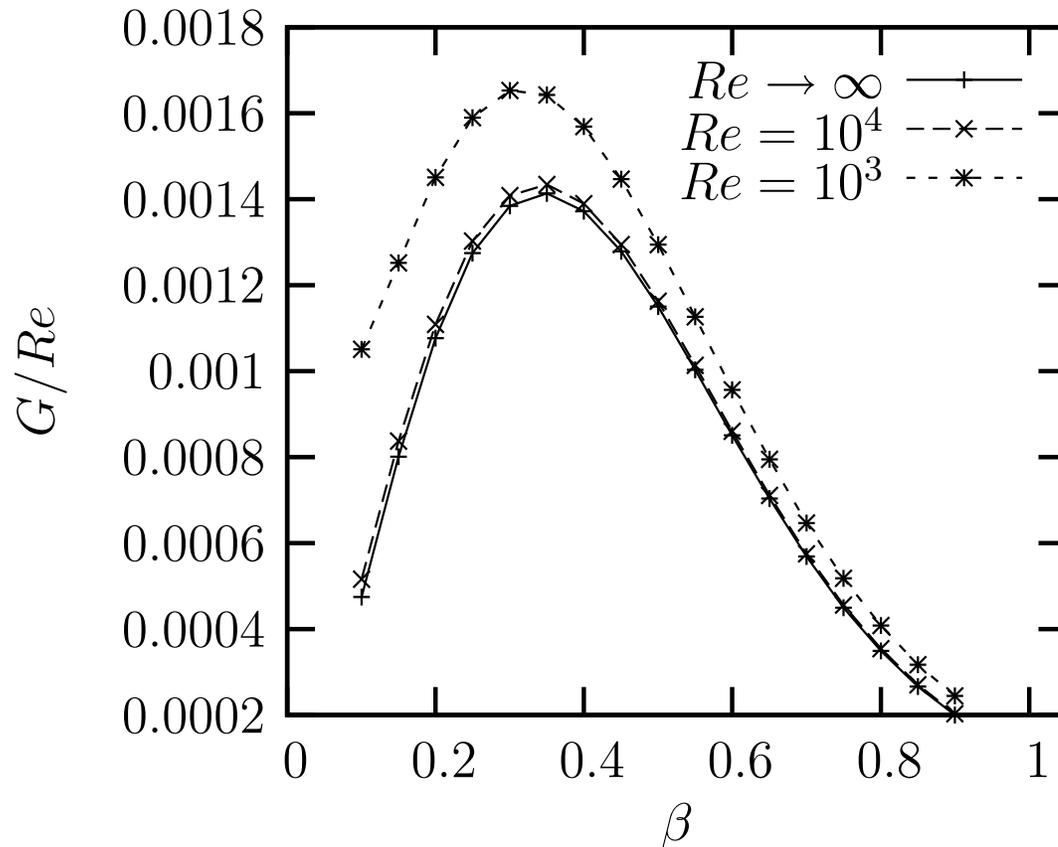
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 - FEN depends on Re , PEN is Re -independent.

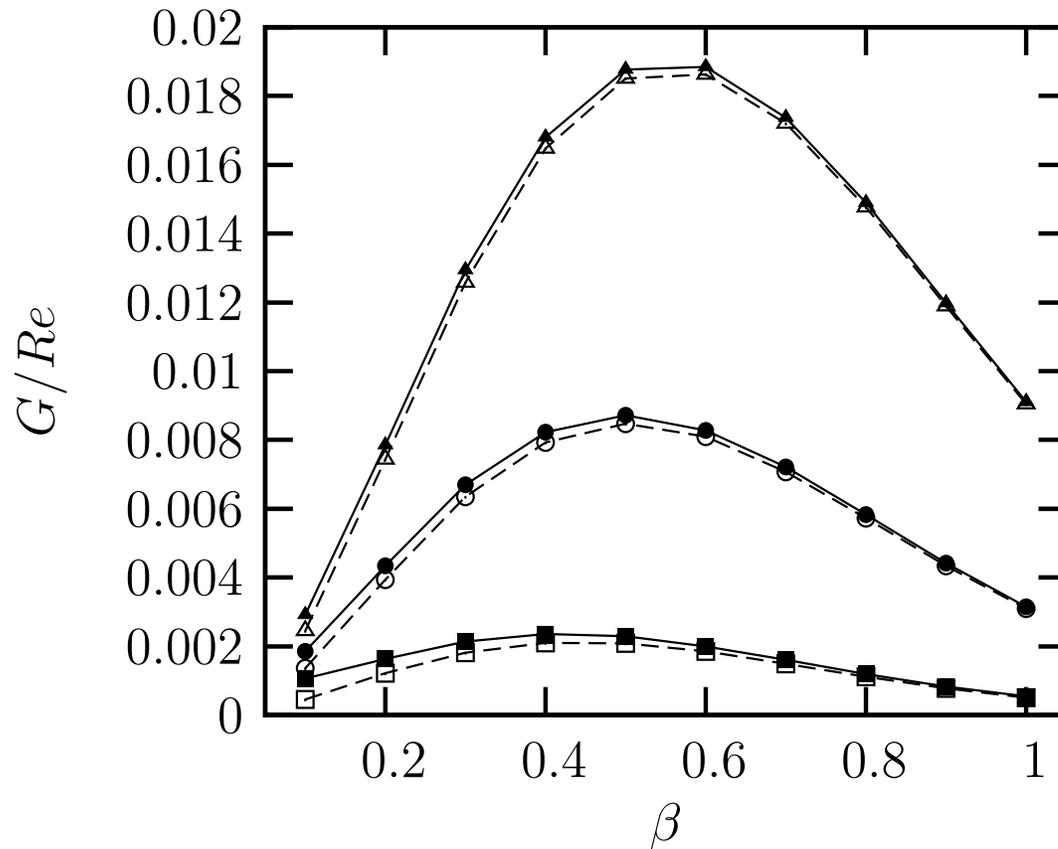
Results – Flat plate



Objective function G/Re : effect of Re and β for $M = 3$, $T_w/T_{ad} = 1$, $x_{in} = 0$ $x_{out} = 1.0$, FEN.

\Rightarrow Reynolds number effects only for $Re < 10^4$.

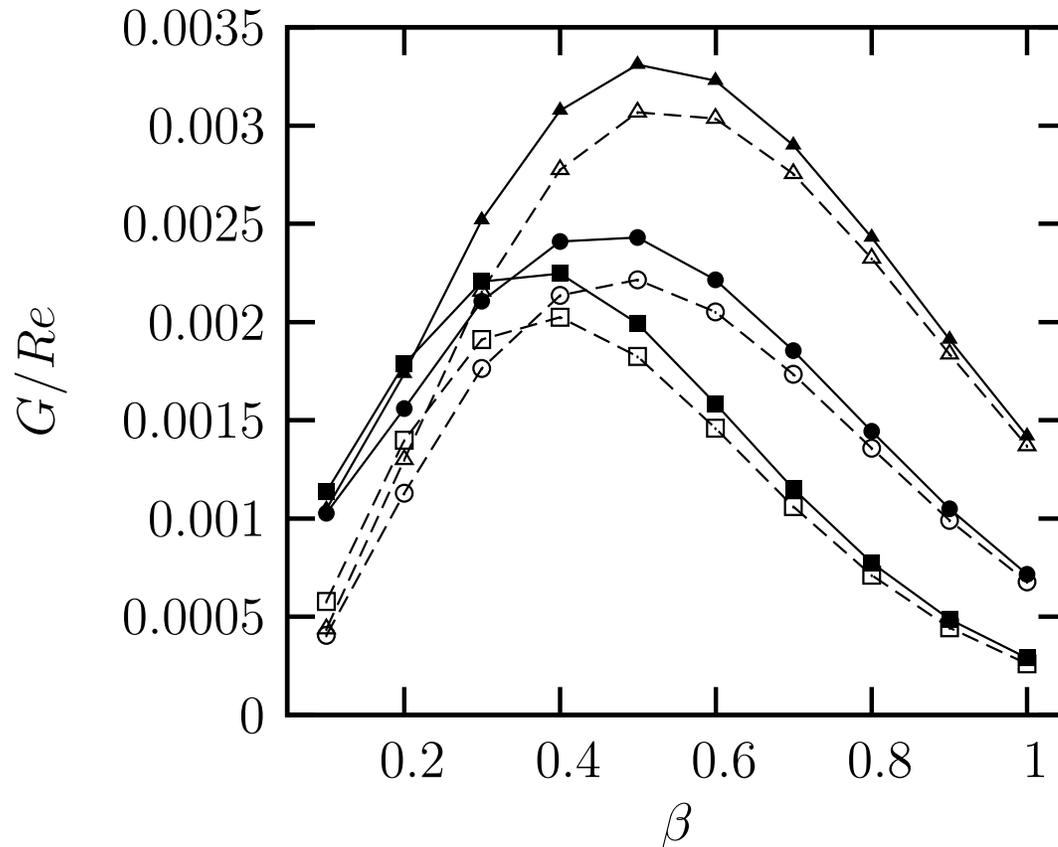
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Objective function G/Re : effect of β , T_w/T_{ad} and norm choice (PEN vs. FEN) for $M = 0.5$, $Re = 10^3$, $x_{in} = 0$ $x_{out} = 1.0$. \square , $T_w/T_{ad} = 1.00$; \circ , $T_w/T_{ad} = 0.50$; Δ , $T_w/T_{ad} = 0.25$.

\Rightarrow No remarkable norm effects; cold wall destabilizing factor.

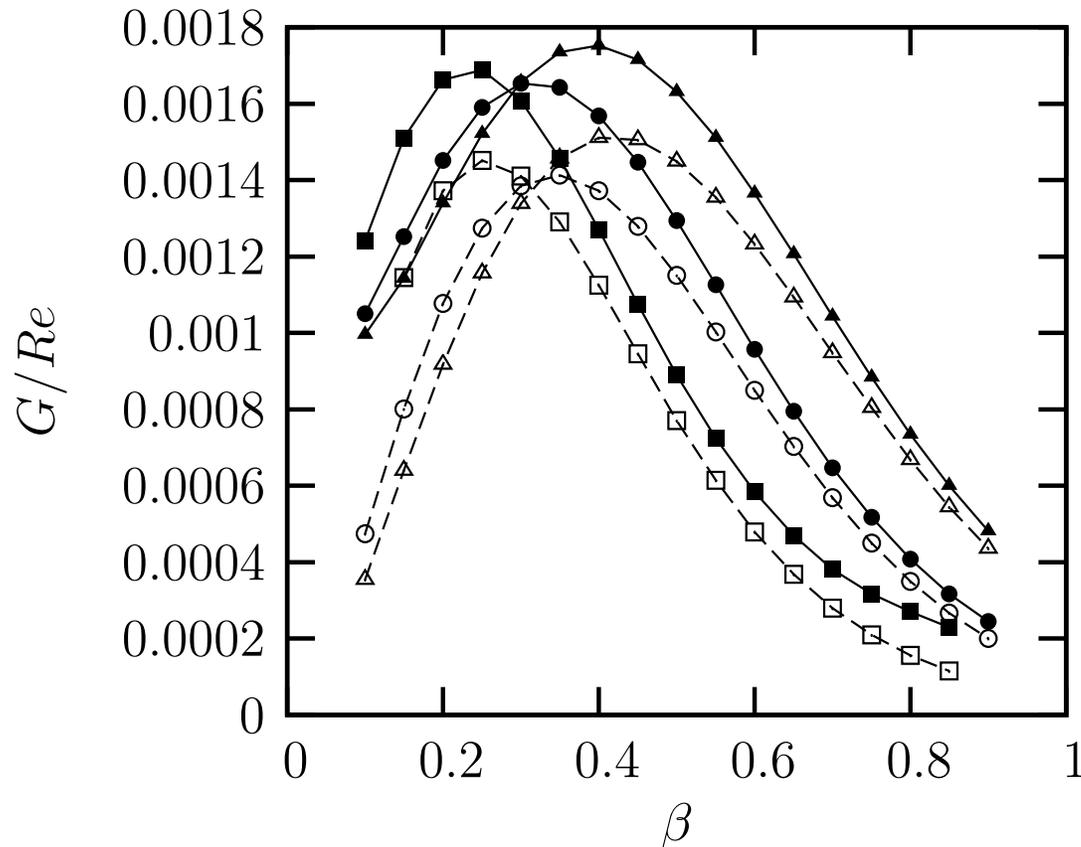
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\Rightarrow Shift of the curves maximum, enhanced difference between norms ($T_w/T_{ad} = 1.00$).

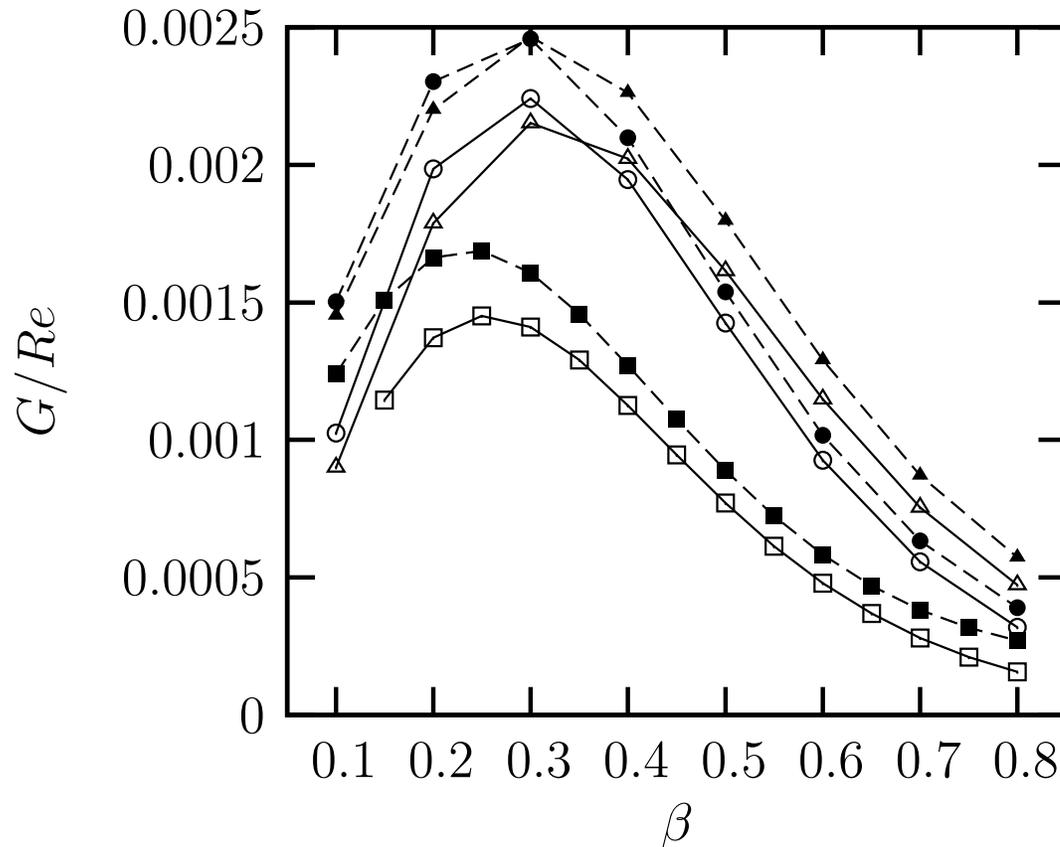
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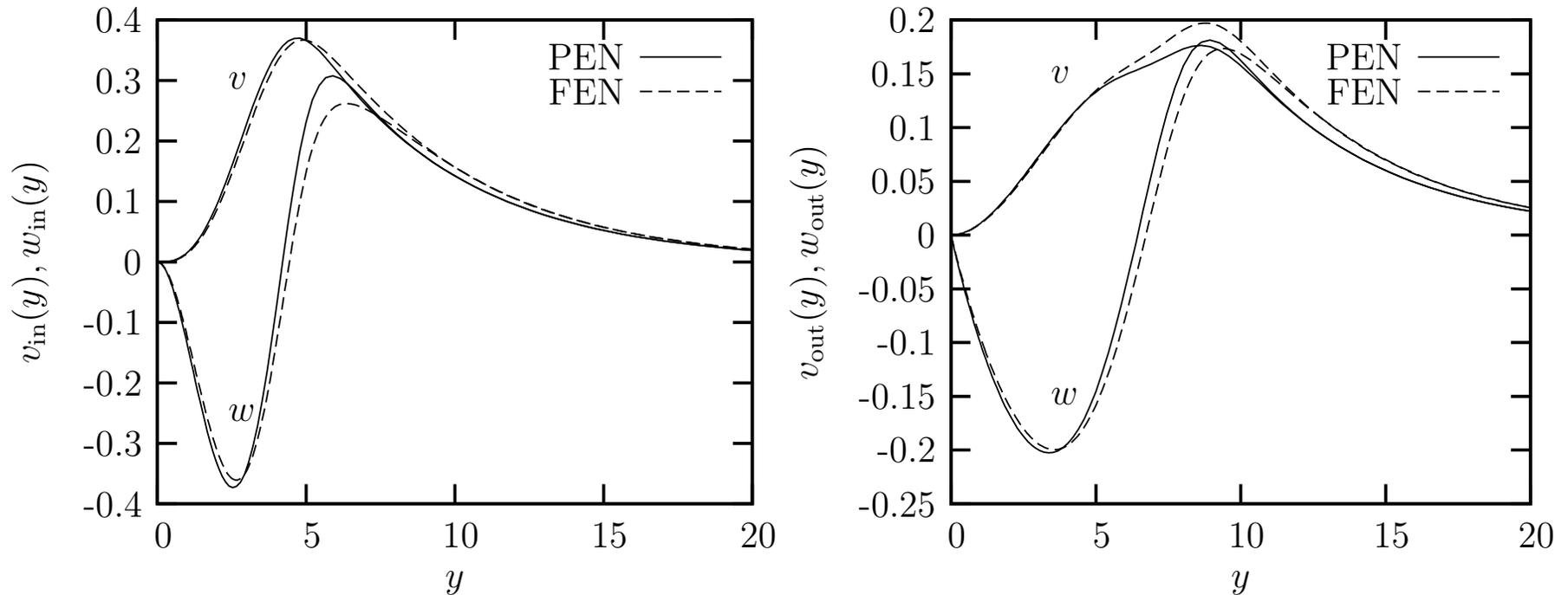
\Rightarrow Up to 17% difference for low values of β .

Results – Flat plate



Objective function G/Re : effect of x_{in} and β and norm choice (PEN vs. FEN) for $M = 3$, $T_w/T_{ad} = 1$, $x_{out} = 1.0$. \square , $x_{in} = 0.0$; \circ , $x_{in} = 0.2$; Δ , $x_{in} = 0.4$.
 \Rightarrow Up to 60% difference for $x_{in} = 0.4$ and $\beta = 0.1$.

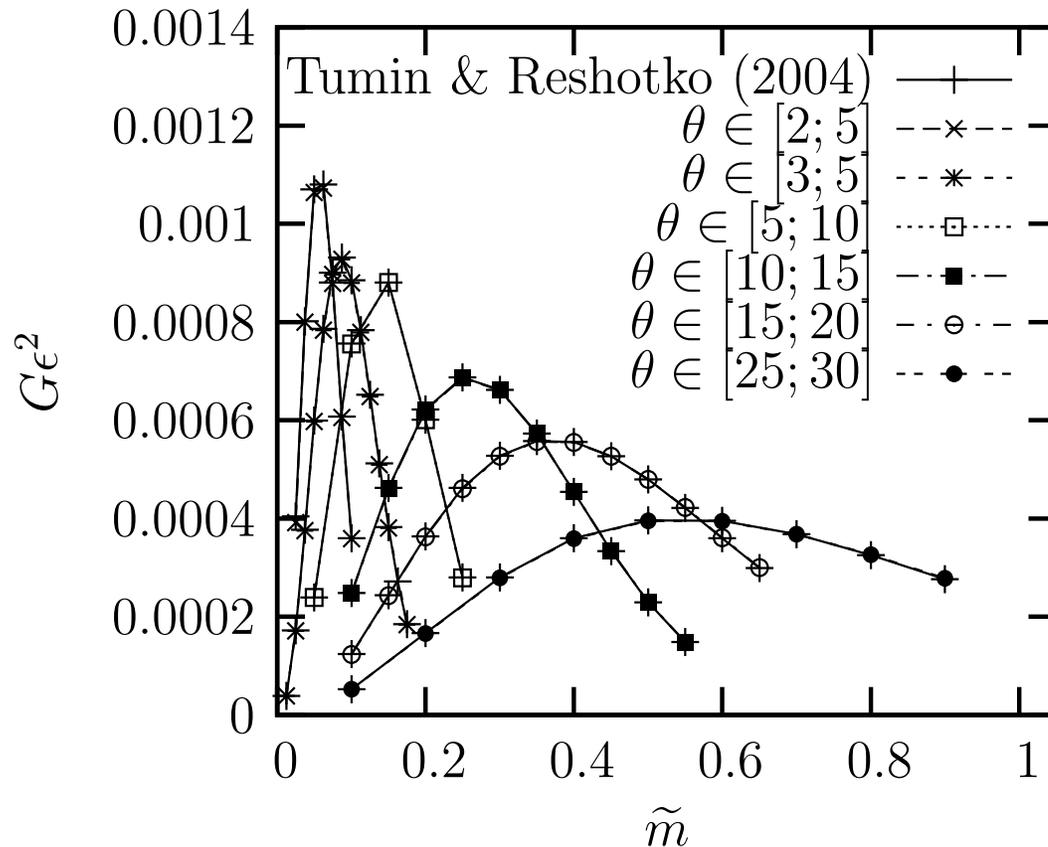
Results – Flat plate



Inlet and outlet profiles: effect of norm choice (PEN vs. FEN) for $M = 3.0$, $Re = 10^3$, $x_{in} = 0.4$, $x_{out} = 1.0$ and $\beta = 0.1$.

⇒ No significant changes in v_{in} , some discrepancies in w_{in} ; larger effects on v_{out} , rather than on w_{out} . No significant effects on u_{out} and T_{out} .

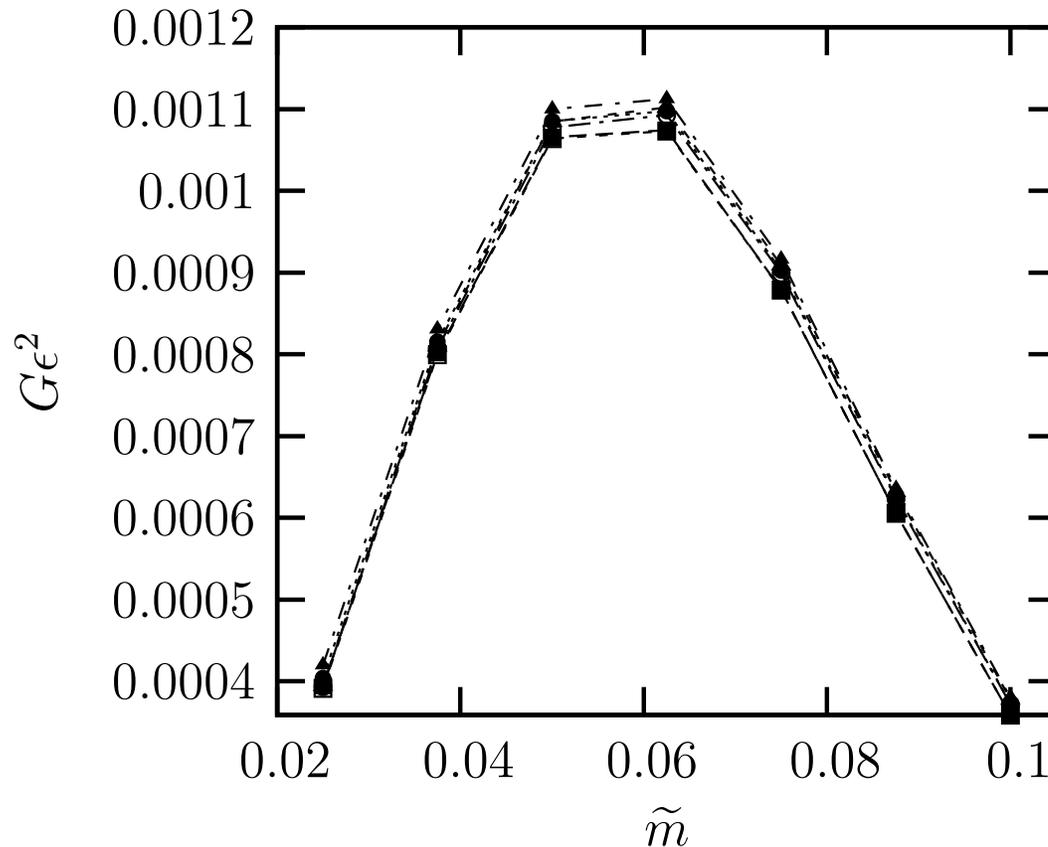
Results – Sphere



Objective function $G\epsilon^2$: effect of interval location and $\tilde{m} = m\epsilon$ for $\theta_{\text{ref}} = 30.0$ deg,
 $T_w/T_{\text{ad}} = 0.5$, $\epsilon = 10^{-3}$. **PEN.**

⇒ Largest gain for small $\theta_{\text{out}} - \theta_{\text{in}}$; strongest transient growth close to the stagnation point.

Results – Sphere



Objective function $G\epsilon^2$: effect of ϵ , energy norm (PEN vs. FEN) and $\tilde{m} = m\epsilon$ for $\theta_{\text{in}} = 2.0$ deg, $\theta_{\text{out}} = 5.0$ deg, $\theta_{\text{ref}} = 30.0$ deg, $T_w/T_{\text{ad}} = 0.5$. \square , $\epsilon = 1 \cdot 10^{-3}$; \circ , $\epsilon = 2 \cdot 10^{-3}$; \triangle , $\epsilon = 3 \cdot 10^{-3}$.

⇒ Maximum appreciable difference within 1%. Effect increases with ϵ .

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- ✓ Sphere. Largest $G\epsilon^2$ close to the stagnation point and for small range of θ . No significant role played by v_{out} and w_{out} in the interesting range of parameters.

The End!

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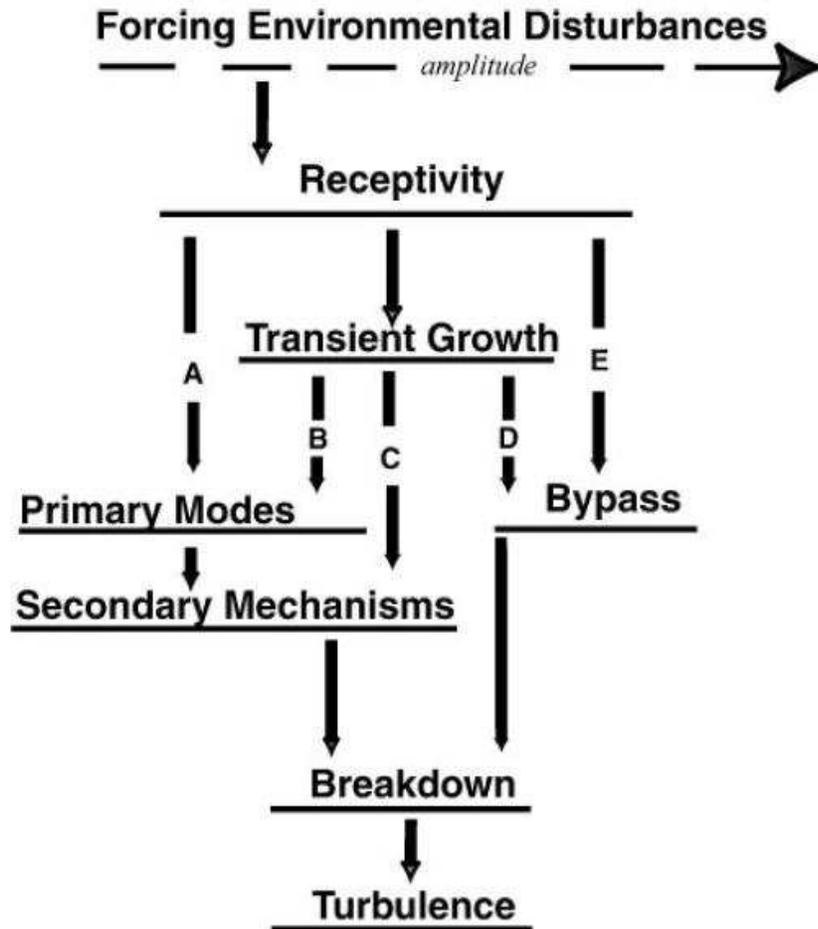
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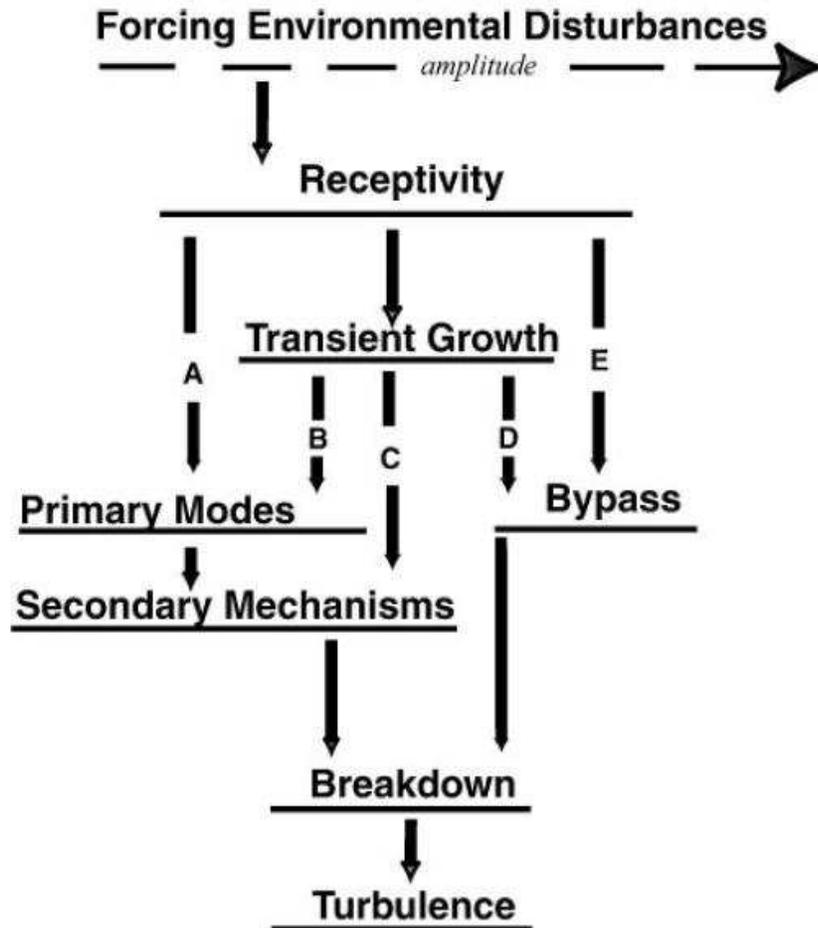
There must exist another mechanism, not related to the eigenvalue analysis: **transient growth**.

Alternative paths of BL transition



M. V. Morkovin, E. Reshotko, and T. Herbert, (1994), "Transition in open flow systems – A re-assessment", *Bull. Am. Phys. Soc.* **39**, 1882.

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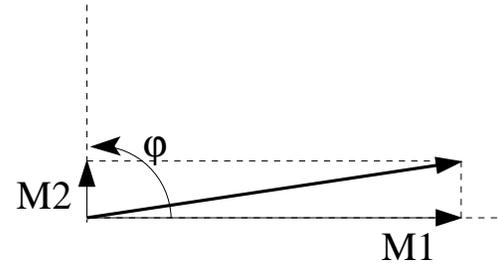
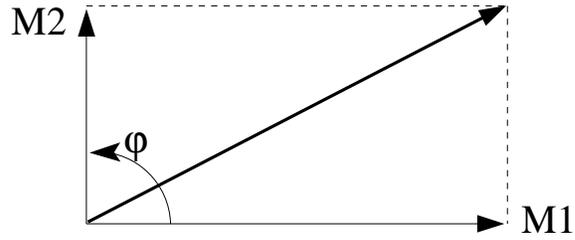


“At the present time, **no mathematical model exists that can predict the transition Reynolds number on a flat plate**”!

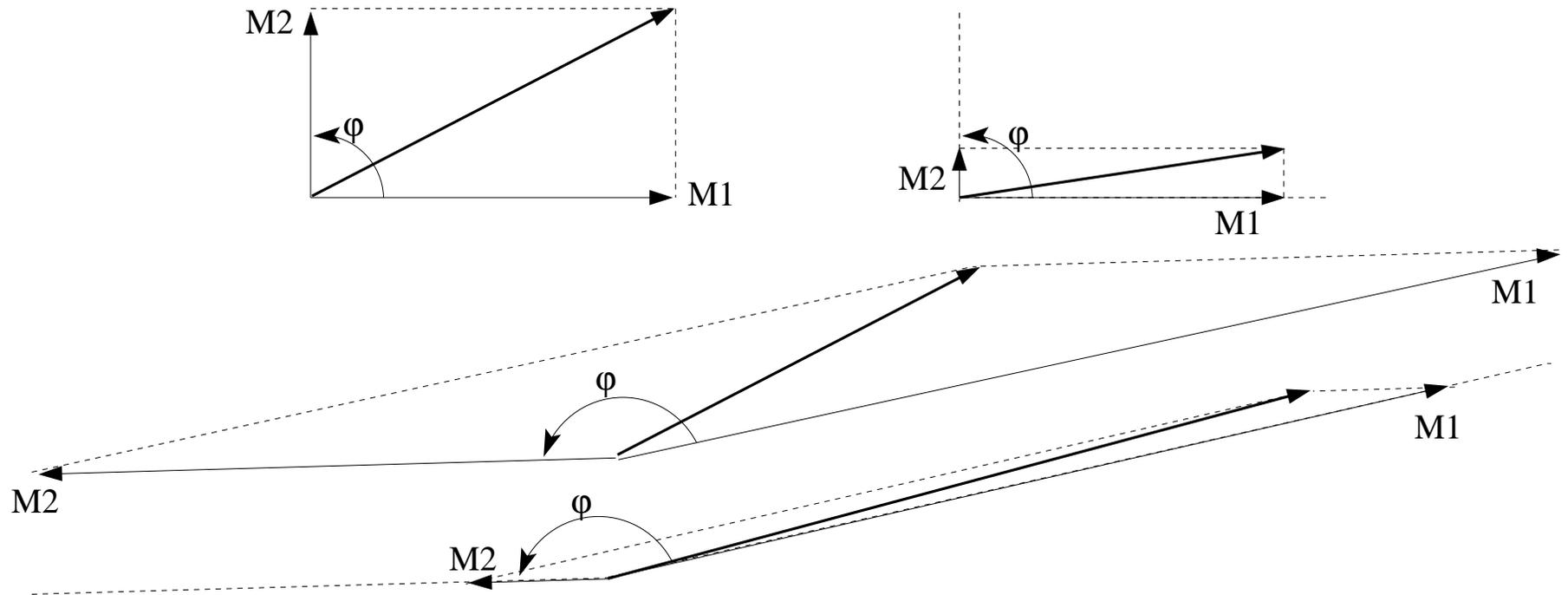
Saric et al., *Annu. Rev. Fluid Mech.* 2002. **34**:291–319

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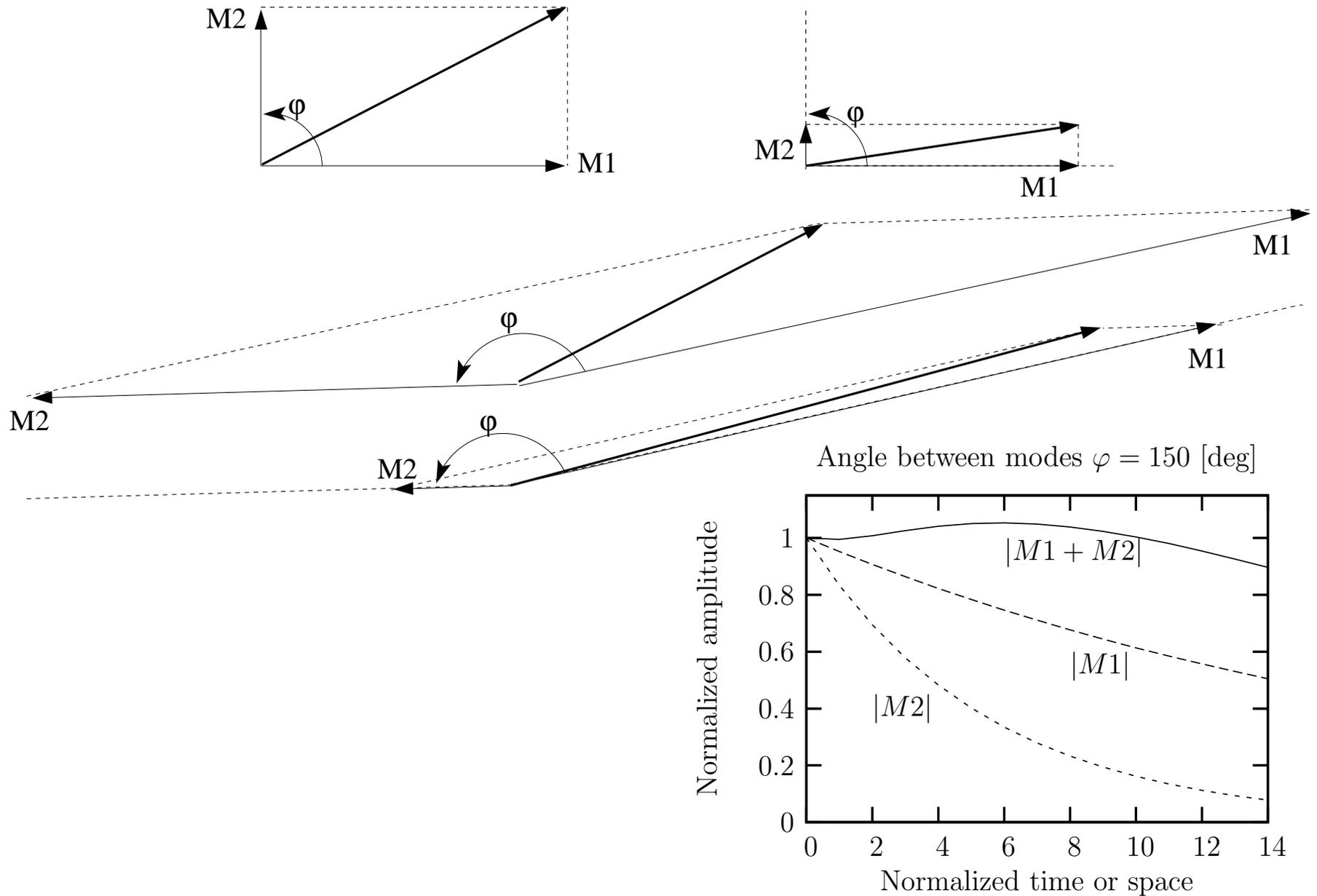
Transient growth



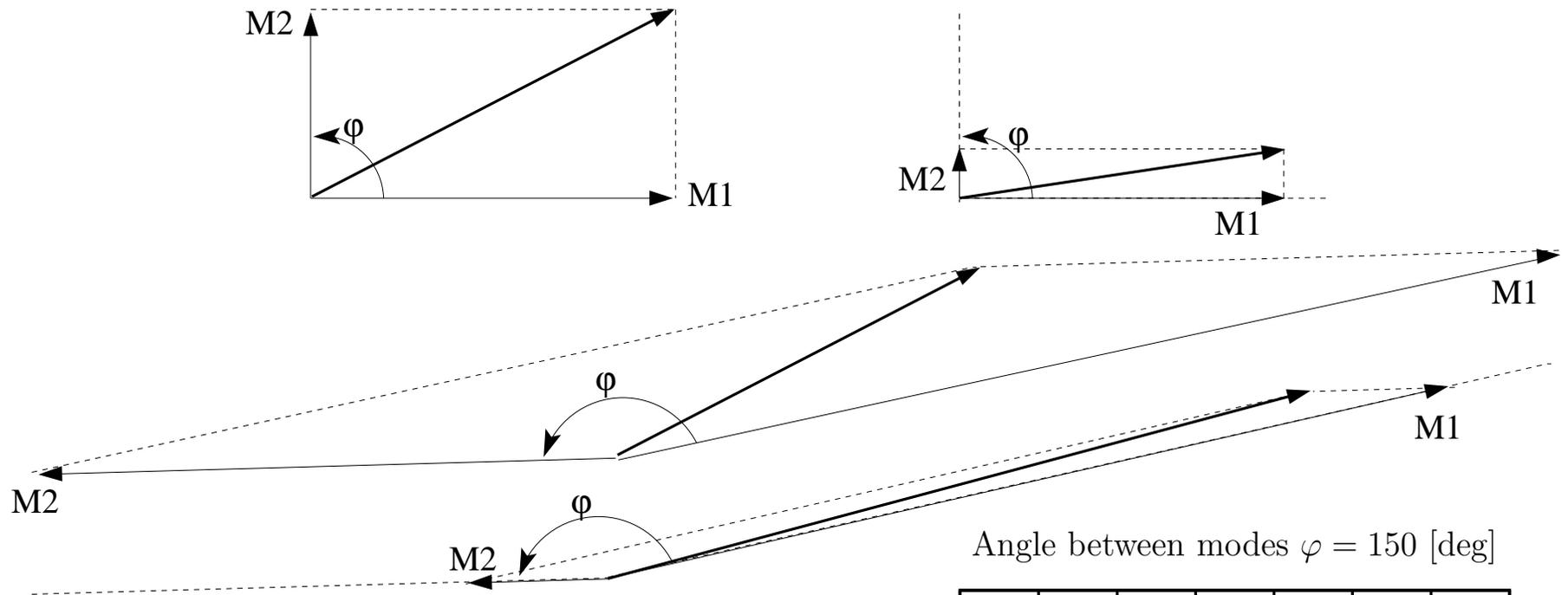
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Transient growth



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Non-normality of the operator. For most flows the linear stability equations are not self-adjoint (the eigenfunctions are not orthogonal)

